

# How Wicks and Orientation

## Affect Heat Pipe Performance

A heat pipe is a device with very high thermal conductance that can transport large quantities of heat with small temperature difference between its hot and cold ends. It is normally used to transport heat from one area to another or to smooth the temperature distribution on a solid surface. Heat pipes are widely used in aerospace applications, military devices, temperature control systems, and now in personal computers.

A heat pipe is a self-driven, two-phase device. A schematic view is shown in Figure 1. At its hot end (evaporator) the liquid evaporates and turns to vapor. This vapor flows to the cold end (condenser) where it liquefies. The liquid is driven back from the cold end to the hot end by capillary forces within the heat pipe's wick structure.

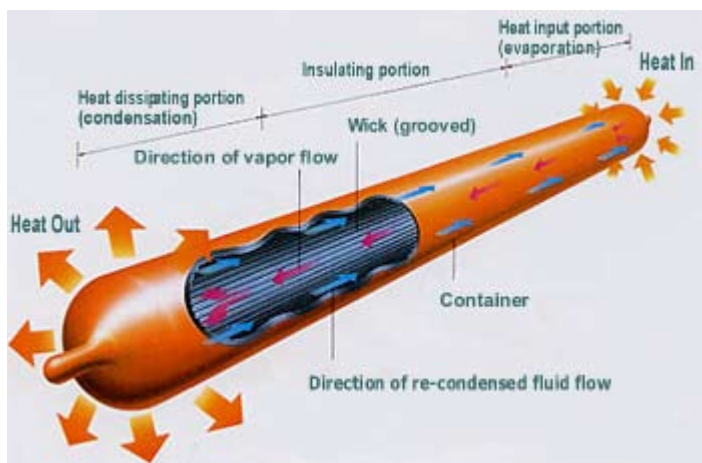


Figure 1. Typical Heat Pipe [1].

The heat transfer ability of a heat pipe is determined by its

diameter, fluid type, wick structure, and orientation. The heat flux limitations of a heat pipe are governed by the following factors (Figure 2):

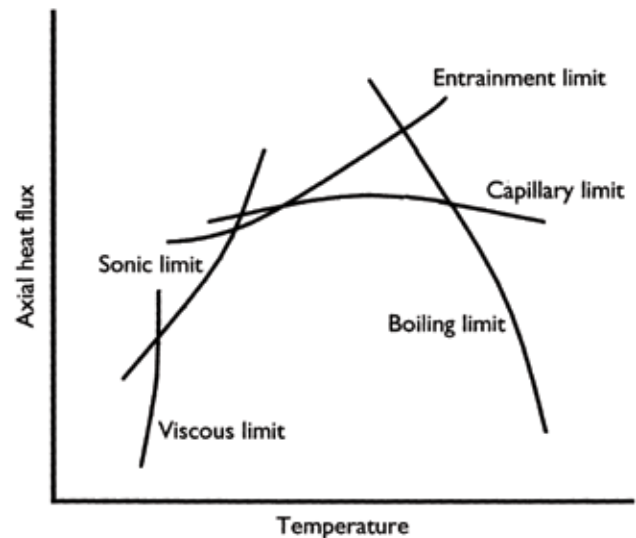


Figure 2. Limits to Heat Transfer in a Heat Pipe [2].

- 1) Viscous Limit. At low temperature, the vapor pressure difference between the evaporator and the condenser may not be enough to overcome viscous forces.
- 2) Sonic Limit. This occurs when the vapor velocity reaches sonic speed at the evaporator and any increase in the pressure difference will not speed up the flow.
- 3) Entrainment Limit. At high vapor velocities, droplets of liquid are torn from the wick and entrained in vapor. The droplets flow to the condenser with the vapor, which results in drying out on the evaporator.
- 4) Capillary Limit. This is reached when the capillary

pressure is too low to transport enough liquid to the evaporator from the condenser.

- 5) Boiling Limit. When the radial heat flux into the heat pipe causes the liquid in the wick to boil and evaporate, which leads to heat pipe dry out.

For a heat pipe to operate, the capillary pumping power  $\Delta P_{capillary}$  must be greater than the total pressure drop in the pipe. The total pressure drop is made up of three components [2]:

- 1) The pressure drop  $\Delta P_v$  required to drive the vapor to flow from evaporator to condenser.
- 2) The pressure drop  $\Delta P_l$  needed to pump the liquid back to the evaporator from the condenser.
- 3) The pressure from the gravitational head,  $\Delta P_g$ , which can be zero, positive or negative, depending on the relative location of the evaporator and condenser.

For the fluid inside a heat pipe to circulate, the following equation must be satisfied:

$$\Delta P_{capillary} \geq \Delta P_v + \Delta P_l + \Delta P_g$$

If this condition is not met, the wick on the evaporator will dry out and the heat pipe will overheat. The maximum allowable heat flux  $\Delta P_{capillary\_max}$  is referred to as the capillary limit. In typical operating conditions, the capillary limit determines the maximum heat transfer rate of the heat pipe.

For a heat pipe, the pumping power  $\Delta P_{capillary}$  occurs on the gas and liquid interface of the wick structure due to surface tension differences. Pore radius and permeability are the two most important characteristics of a wick structure. The pore radius determines the pumping pressure that the wick can develop. The smaller the pore radius, the larger the pumping power. The permeability determines the fractional pressure losses of the working fluid  $\Delta P_l$ . The pressure drop  $\Delta P_v$  is directly related to the rate of vapor traveling from the evaporator to the condenser.

The heat transfer rate is also affected by the diameter and the length of the heat pipe. In a large diameter heat pipe, the cross sectional area will allow higher vapor volume to

be transported from the evaporator to the condenser than in a small diameter pipe. The cross sectional area of a heat pipe affects the sonic limit and entrainment limit, as well. In general, heat pipes with larger diameters transport more heat. The gravitational pressure head  $\Delta P_g$  is determined by the relative positions of the evaporator and condenser. If the angle between a straight heat pipe and horizontal is  $f$  ( $f$  is positive when the evaporator is lower than condenser), the gravitational pressure head  $\Delta P_g$  can be calculated as follows:

$$\Delta P_g = - \rho_l g l \sin \theta$$

Where  $\rho_l$  is liquid density and  $l$  is heat pipe length.

The most commonly used wick structures for heat pipes are simple and homogeneous, such as grooves, wire mesh, sintered metal powders, and fiber. Other composite wick structures are included in Figure 3 [2]. Each wick structure has its advantages and disadvantages.

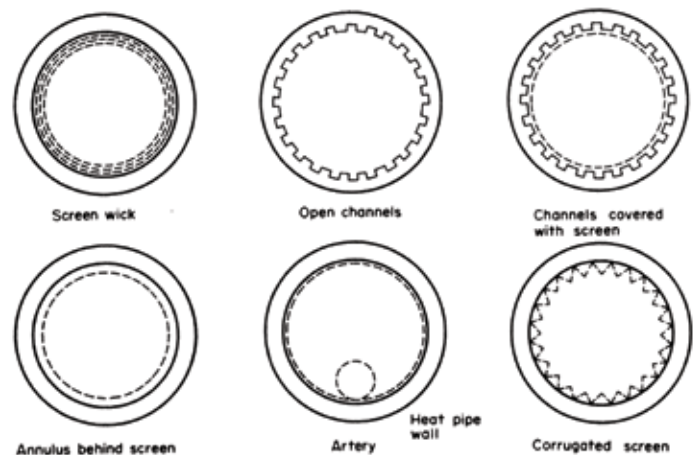


Figure 3. Heat Pipe Wick Structures [2].

The HP-1 is a series of high performance, sintered wick structure heat pipes produced by Thermacore. These pipes are available in diameters of 6.35 mm (1/4 in), 9.52 mm (3/8 in), 12.7 mm (1/2 in) and 15.89 mm (5/8 in). Thermacore Corporation tested these 304.8 mm (12 in) long heat pipes with 76.2 mm (in) evaporator and 76.2 mm (3 in) condenser sections at a 100°C operating temperature. The results are



# CLWT-067

## BENCHTOP, CLOSED LOOP WIND TUNNEL FOR ELEVATED TEMPERATURE TESTING OF BOARDS AND COMPONENTS

The CLWT-067 is a research-quality closed loop wind tunnel that provides a convenient, accurate system for thermally characterizing PCBs and individual components at controlled temperatures from ambient to 85°C.

The CLWT-067 wind tunnel produces air flows up to 7 m/s (1378 ft/min). With customization, it can generate flows up to 50 m/s (10,000 ft/min) using orifice plates (available optionally). The clear Lexan test section lets the user to view the test specimen and allows for flow visualization.

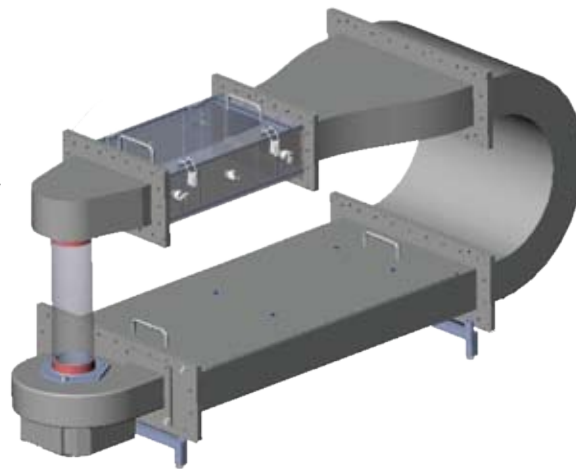
Unlike open loop wind tunnels, the CLWT-067 re-circulates internal air. This allows the system heater to quickly warm the air to a specific temperature. The testing of boards and components in hot air is a requirement in some NEBS and other standards. The precise controls and temperature range of the CLWT-067 wind tunnel allows its use for testing heat sink performance and for calibrating air and temperature sensors.

The complete wind tunnel fits on most lab benches and is powered from standard AC outlets. It has a smaller footprint than traditional, closed loop wind tunnels or environmental test chambers.

The wind tunnel's test section can be accessed from the top door for mounting and repositioning of boards, components and sensors. Internal rail guides provide an easy mechanism to install test specimens of different sizes (e.g., PCB, heat sink).

Instrument ports (6) are provided in the side walls of the test section for placing temperature and velocity sensors such as thermocouples, Pitot tubes and hot-wire anemometers.

Custom options are also available. Contact ATS for details.



### OVERALL DIMENSIONS (L X W X H)

143.6 cm x 49.3 cm x 67.7 cm  
(56.5" x 19.4" x 26.6")

### TEST SECTION DIMENSIONS

41.8 cm x 22.5 cm x 9.5 cm  
(16.4" x 8.9" x 3.7")

### MATERIALS

SHEET METAL, LEXAN

### FLOW RANGE

0 TO 7 m/s (1378 ft/min)

### TEMPERATURE RANGE

Up to 85°C (185°F)

### WEIGHT

70.7 kg (156 lbs.)

### FEATURES:

#### » Quick Access

Quickly change the test specimen through the top access test section

#### » Sensor Ports

Measure pressure, velocity and temperature through the sensor ports

#### » Data Center

View data and monitor events (with optional controller)

#### » Flow Characteristics

High quality flow with very low turbulence intensity

### APPLICATIONS:

#### » High Temperature Testing

Evaluate the effects of elevated temperatures on component and PCB response and reliability

#### » Heat Sink Characterization

Characterize a variety of heat sink sizes for natural and forced convection cooling

#### » Sensor Calibration

Precision temperature and velocity controls allow accurate calibration of sensors

#### » Component Testing

Utilize for individual or multiple component testing

#### » Multiple PCB Testing

Test actual or simulated PCBs for thermal and flow distribution

For further technical information, please contact Advanced Thermal Solutions, Inc. at **1-781-769-2800** or **www.qats.com**

presented in Figures 4 and 5 [3].

Figure 4 shows the temperature difference between evaporator and condenser at different power levels when the heat pipes are vertical. Compared to small diameter heat pipes, large diameter heat pipes transport more heat with the same  $\Delta T$ . Figure 5 illustrates the relationship between power and the inclination angle for different heat pipes. Clearly the sintered wick structure pipes are better with the help of gravity. When the inclination angle is larger than  $10^\circ$ , the heat flux that the heat pipes can transport does not vary much. As the inclination angle gradually decreases from  $10^\circ$ , the heat flux decreases as well. At a  $-90^\circ$  angle, the heat flux is less than half of that at  $10^\circ$ .

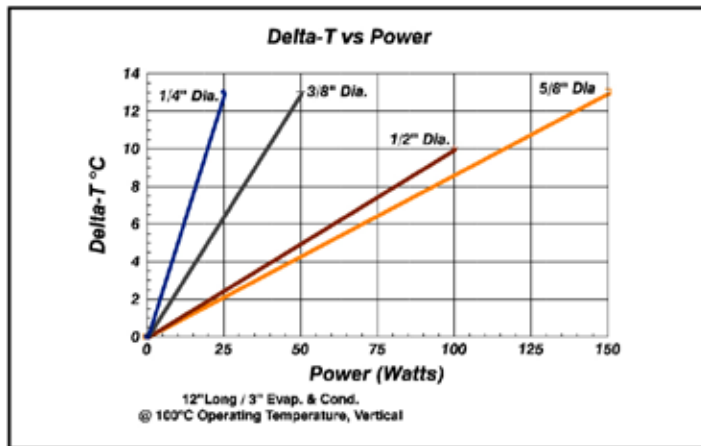


Figure 4. HP-1 Delt-T vs. Power [3].

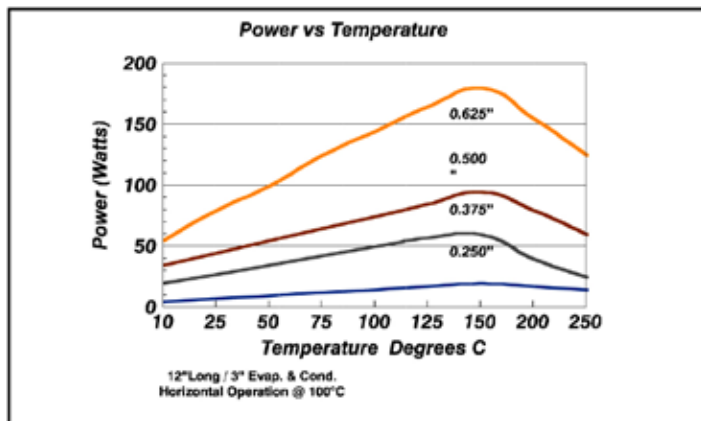


Figure 5. HP-1 Power vs. Angle [3].

Loh et al [4] experimentally studied the effects of wick structure and orientation on heat pipe performance. The bench they used for the tests is shown in Figure 6. The heat pipes they tested were 4 mm, 5 mm, and 6 mm in diameter. The pipes were 200 mm long with a 35 mm evaporator and a 35 mm condenser. Each test started with an inclination angle  $\theta$  of  $90^\circ$ , the vertical position at which the evaporator block was located at the bottom. The tests ran through a  $180^\circ$  rotation that paused at each of the following inclination angles:  $60^\circ$ ,  $30^\circ$ ,  $0^\circ$  (horizontal),  $-30^\circ$ ,  $-60^\circ$  and  $-90^\circ$ .

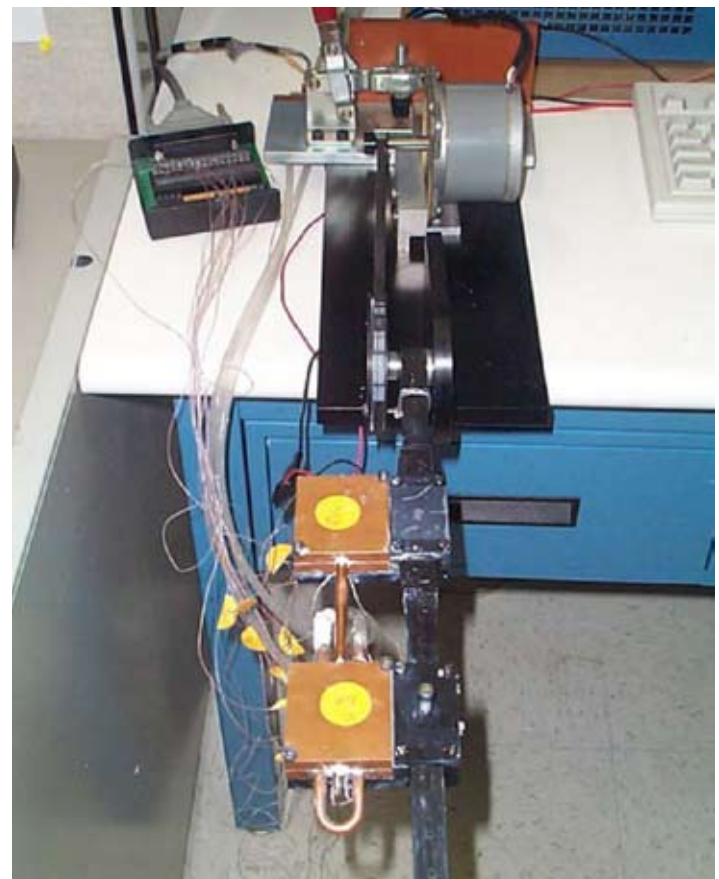
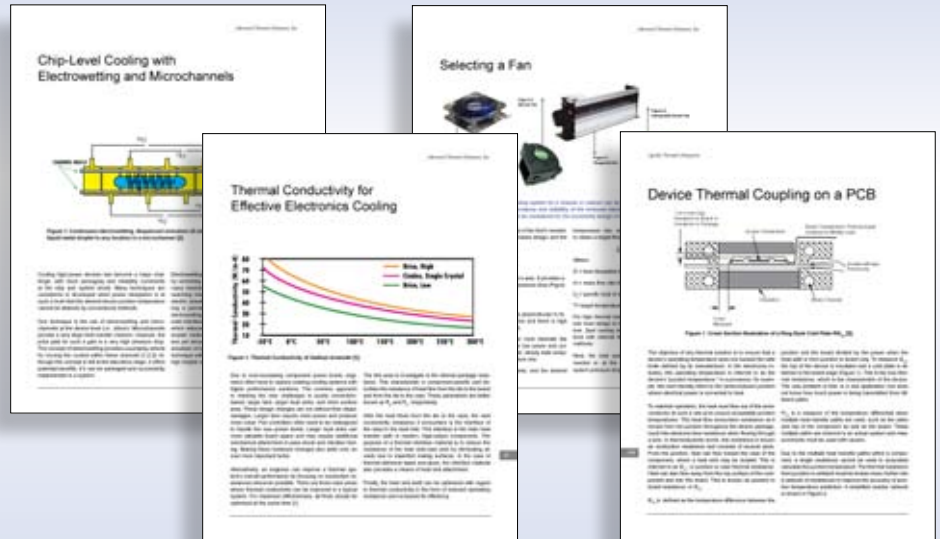


Figure 6. Photo of Heat Pipe Test Bench [4].

Figures 7, 8 and 9 show the temperature differences between evaporator and condenser for mesh, groove and sintered metal powder heat pipes, respectively. A heat pipe with a mesh wick structure has the largest thermal impedance. The orientation has a large effect on its heat transfer, but it manages to work at low and moderate heat flux even at a  $-90^\circ$  angle. A heat pipe with a groove wick has the smallest

# First Volume of Qpedia Thermal eMagazine Articles Now Available in Hardcover Book



**\$94.95**  
On Sale Now!

Visit [www.qats.com](http://www.qats.com), email [qpedia@qats.com](mailto:qpedia@qats.com) or call 781-769-2800 to place your order!

Advanced Thermal Solutions, Inc. (ATS) has published Qpedia Thermal eMagazine, Volume 1, Issues 1-12, a hardbound, full-color book that compiles all of the electronics thermal management articles that first appeared in its online emagazine, Qpedia. In all, the book contains 46 technically comprehensive articles offering expert-level coverage on a wide range of heat management issues that impact virtually all of today's electronic devices. Topics range from spot cooling hot areas on silicon dies to enhancing airflow over PCBs and inside chassis and cabinets.

All articles are written and edited at the engineer-level by the thermal and mechanical engineers from Advanced Thermal Solutions, including Kaveh Azar, Ph.D., the company's president and CEO; and Bahman Tavassoli, Ph.D., its chief technologist. Both Azar and Tavassoli are internationally recognized experts in the thermal management of electronics.

Qpedia Thermal eMagazine, Volume 1, Issues 1-12, ISBN-978-0-615-23660-5, the hardbound, full color book can be ordered for \$94.95 (USD) by calling 781-769-2800 or by email [qpedia@qats.com](mailto:qpedia@qats.com).

Volume discounts for organizations and academic institutions are also available. Contact ATS or visit [www.qats.com](http://www.qats.com) for details.

Advanced Thermal Solutions, Inc.  
89-27 Access Road | Norwood, MA | USA  
T: 781.769.2800 | F: 769.769.2800 | [www.qats.com](http://www.qats.com)



**ATS** ADVANCED  
THERMAL  
SOLUTIONS, INC.  
Innovations in Thermal Management®

thermal impedance among three wick structures when the inclination angle is positive. However, its temperature difference increases dramatically when the inclination angle changes to negative, even at low heat flux. It fails at a negative inclination angle when the heat flux is larger than 15 W. The performance of a heat pipe with sintered metal powder is not affected much by its orientation when the heat flux is less than 15 W. At moderate heat flux, the sintered metal powder heat pipe can still work against gravity with an increased temperature difference. At high heat flux (>25 W), it can only work with help of gravity.

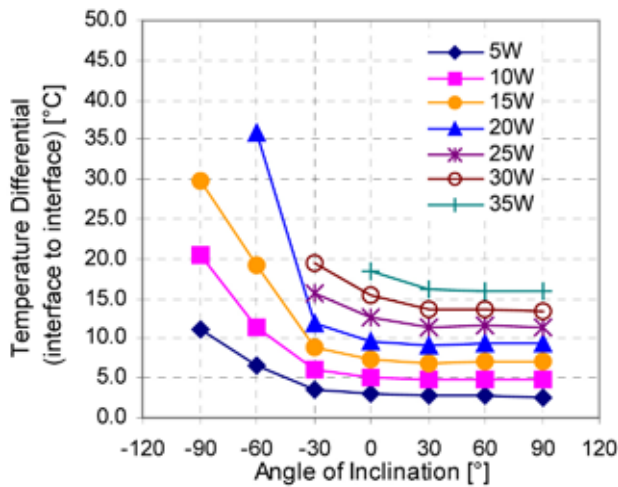


Figure 7.  $\Delta T$  of a 6mm Mesh Heat Pipe at Different Inclination Angles [4].

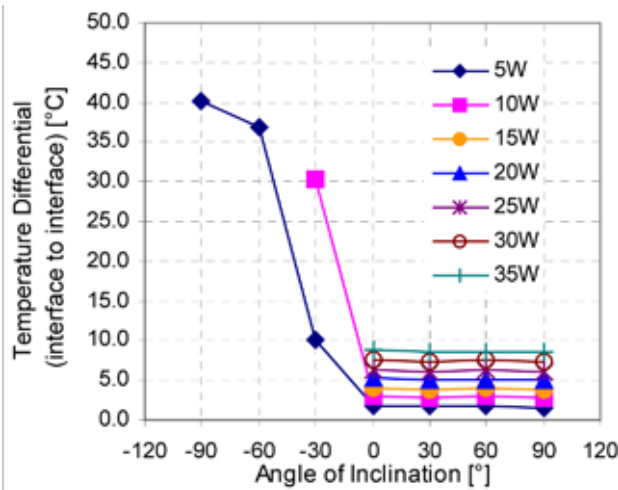


Figure 8.  $\Delta T$  of a 6mm Groove Heat Pipe at Different Inclination Angles [4].

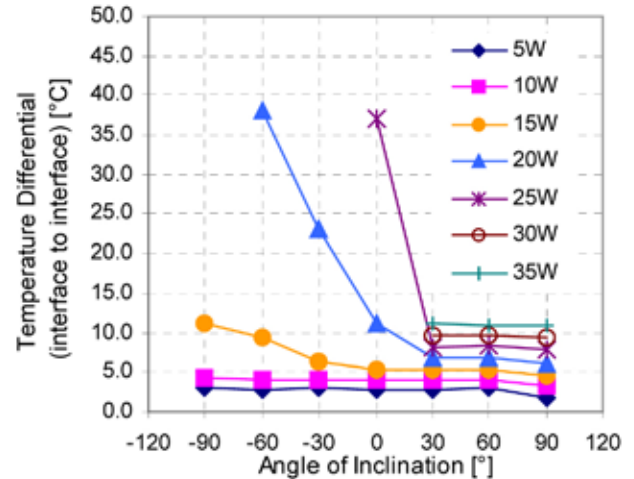


Figure 9.  $\Delta T$  of a 6mm Sintered Metal Powder Heat Pipe at Different Inclination Angles [4].

It is important to select the proper wick structure for heat pipes based on their real application. If a heat pipe works in conditions with favorable gravitational force and a few bends, the grooved wick heat pipe is a good choice because of its superior thermal performance. If a heat pipe has complex geometry and works at a small or negative tilting angle, sintered powder metal is the optimum wick structure. For cooling electronic components in telecommunications devices and computer products, the sintered powder metal wick is the best choice because such applications require a compact heat sink size with many turns and bends. The high capillary pumping pressure achieved by using a sintered powder metal wick due to its small pore size, allows a heat pipe to operate in any orientation. Other wick structures do not work as well in non-vertical orientations because they cannot lift the returning working fluid along the length of the heat pipe against gravity.

#### References:

1. <http://www.lightstreamphotonics.com/technology.htm>
2. Reay, D. and Kew, P., Heat Pipes: Theory, Design and Applications, 5<sup>th</sup> Edition, Butterworth-Heinemann, 2006.
3. HP-1 Heat pipe specification, [www.thermacore.com](http://www.thermacore.com).
4. Loh, C., Harris, E. and Chou, D., Comparative Study of Heat Pipes Performances in Different Orientations, Semiconductor Thermal Measurement and Management Symposium, 2005.