

# TRA2532

## Overvoltage Transient Suppressor

24 V–32 V

Designed for applications requiring a diode with reverse avalanche characteristics for use as reverse power transient suppressor. Developed to suppress transients in automotive system, this device operates in the forward mode as standard rectifier or reverse mode as power zener diode and will protect expensive modules such as ignition, injection, antiblocking system . . . from overvoltage conditions.

- High Power Capability
- Economical

### Mechanical Characteristics

- Finish: All External Surfaces are Corrosion Resistant, and Contact Areas are Readily Solderable
- Polarity: Indicated by Cathode Band
- Weight: 1.8 Grams (Approximately)
- Maximum Temperature for Soldering Purposes: 260°C
- Marking: 2532

### MAXIMUM RATINGS

Rating	Symbol	Value	Unit
DC Blocking Voltage	$V_R$	23	Volts
Average Forward Current (Single Phase, Resistive Load, $T_C = 150^\circ\text{C}$ )	$I_O$	32	Amps
Peak Repetitive Reverse Surge Current (Time Constant = 10 ms, $T_C = 25^\circ\text{C}$ )	$I_{RSM}$	80	Amps
Non–Repetitive Peak Surge Current (Halfwave, Single Phase, 60 Hz)	$I_{FSM}$	500	Amps
Operating Junction Temperature Range	$T_J$	–65 to +175	°C
Storage Temperature Range	$T_{stg}$	–65 to +150	°C



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MICRODE BUTTON  
CASE 193

### MARKING DIAGRAM



2532 = Device Code  
L = Location Code  
YY = Year  
WW = Work Week

### ORDERING INFORMATION

Device	Package	Shipping
TRA2532	Microde Button	5000 Units/Box

# TRA2532

## THERMAL CHARACTERISTICS

Characteristic	Symbol	Value	Unit
Thermal Resistance, Junction to Case	$R_{\theta JC}$	0.8	$^{\circ}C/W$

## ELECTRICAL CHARACTERISTICS

Characteristic	Symbol	Min	Max	Unit
Instantaneous Forward Voltage (Note 1.) ( $i_F = 100$ Amps, $T_C = 25^{\circ}C$ )	$V_F$	–	1.18	Volts
Reverse Current <sup>(1)</sup> ( $V_R = 23$ Vdc, $T_C = 25^{\circ}C$ )	$I_R$	–	10	$\mu A$
Breakdown Voltage <sup>(1)</sup> ( $I_Z = 100$ mA, $T_C = 25^{\circ}C$ )	$V_{(BR)}$	24	32	Volts
Breakdown Voltage ( $I_Z = 80$ Amps, $T_C = 25^{\circ}C$ , $P_W = 80$ $\mu s$ )	$V_{(BR)}$	–	40	Volts
Breakdown Voltage Temperature Coefficient	$V_{(BR)TC}$	0.096*	0.096*	$\%/^{\circ}C$
Forward Voltage Temperature Coefficient @ $I_F = 10$ mA	$V_{FTC}$	–2*	–2*	$mV/^{\circ}C$

1. Pulse Test: Pulse Width  $\leq 300$   $\mu s$ , Duty Cycle  $\leq 2\%$ .

\*Typical

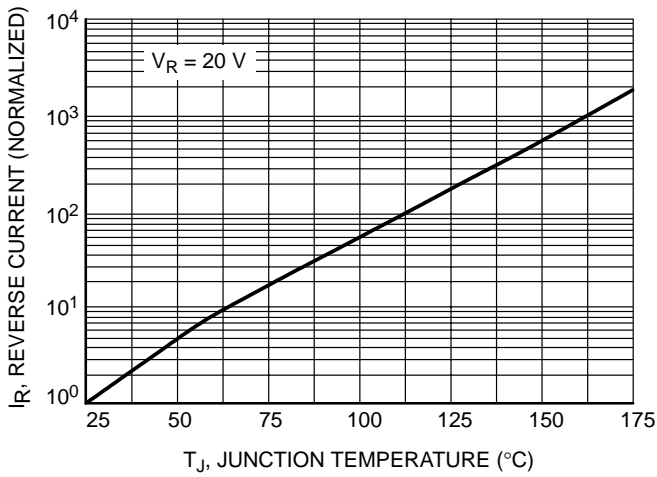


Figure 1. Normalized Reverse Current

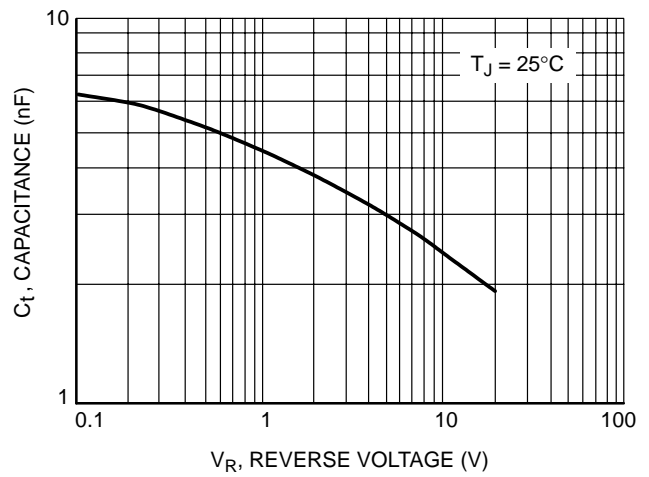


Figure 2. Typical Reverse Capacitance

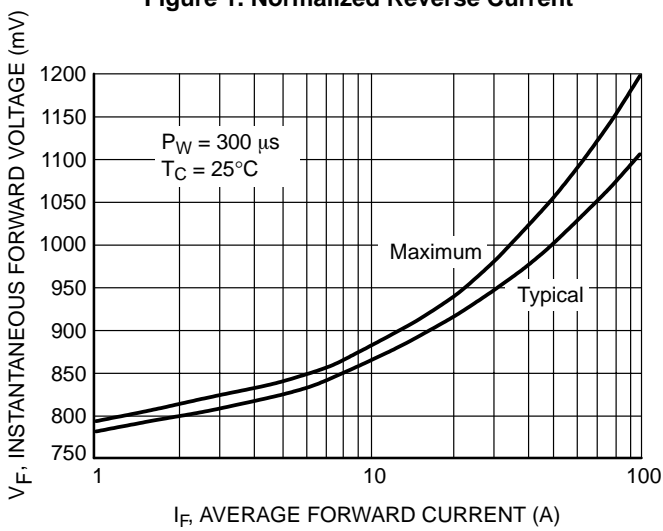


Figure 3. Forward Voltage

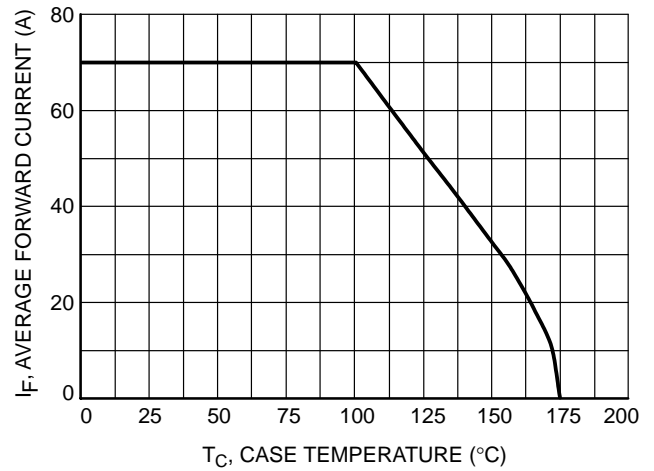


Figure 4. Maximum Current Rating

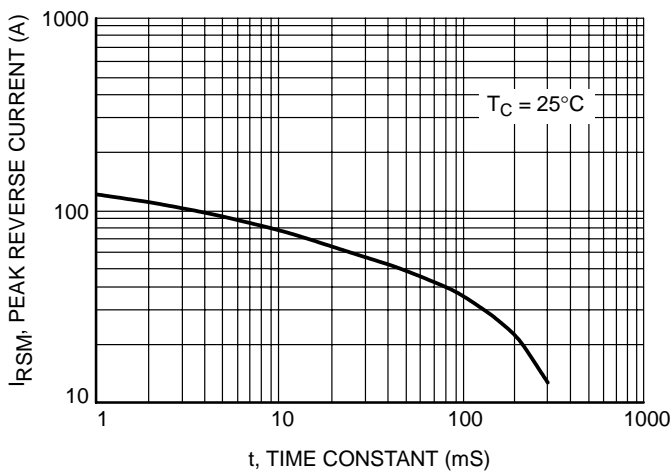


Figure 5. Maximum Peak Reverse Current

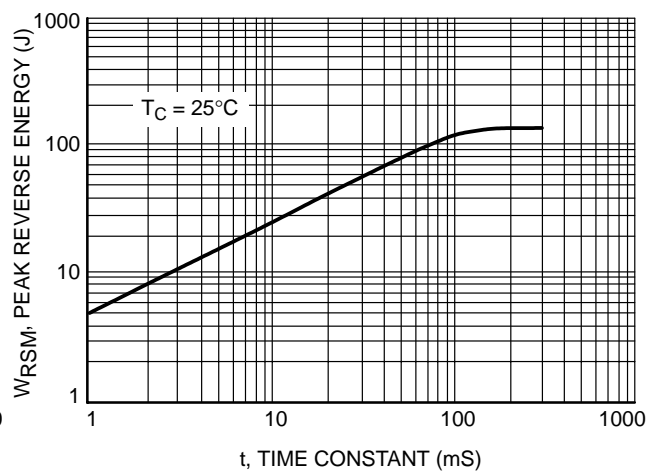


Figure 6. Maximum Reverse Energy

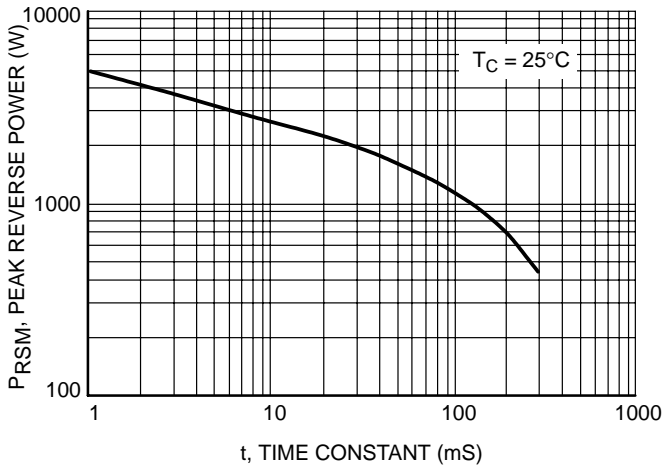


Figure 7. Maximum Peak Reverse Power

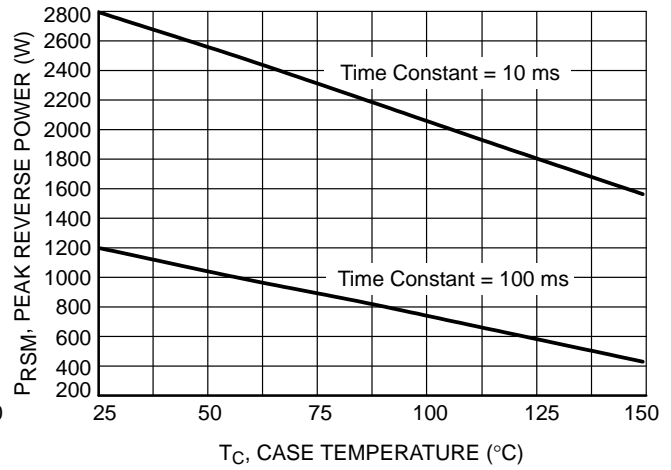


Figure 8. Reverse Power Derating

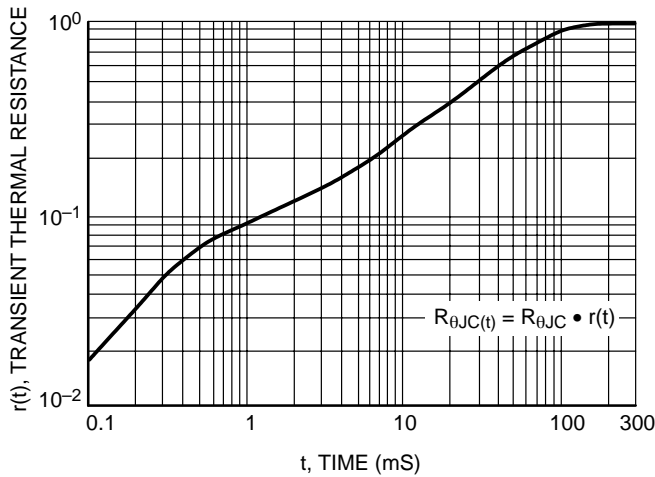


Figure 9. Thermal Response

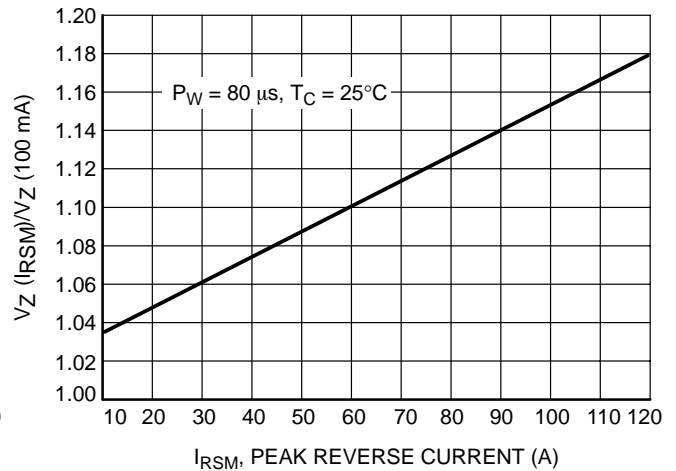
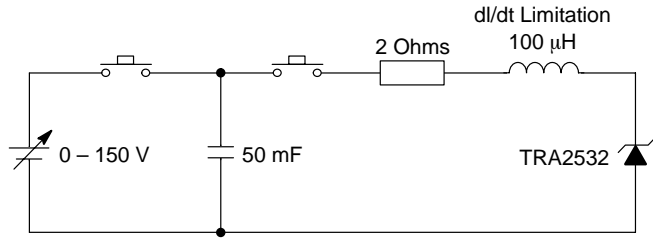
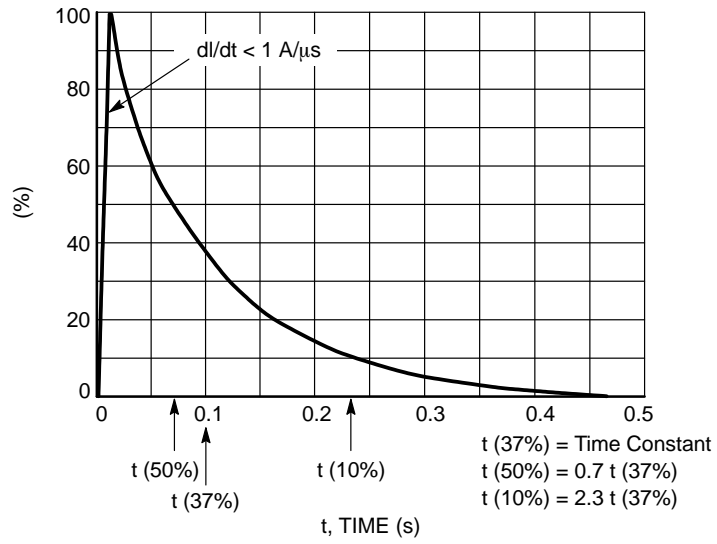


Figure 10. Typical Clamping Factor

# TRA2532



**Figure 11. Load Dump Test Circuit**



**Figure 12. Load Dump Pulse Current**

**Assembly and Soldering Information**

There are two basic areas of consideration for successful implementation of button rectifiers:

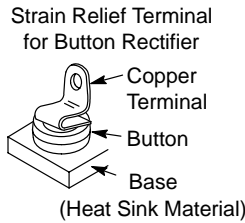
1. Mounting and Handling
2. Soldering

Each should be carefully examined before attempting a finished assembly or mounting operation.

**Mounting and Handling**

The button rectifier lends itself to a multitude of assembly arrangements, but one key consideration must always be included: One Side of the Connections to the Button Must be Flexible!

This stress relief to the button should also be chosen for maximum contact area to afford the best heat transfer – but not at the expense of flexibility. For an annealed copper terminal a thickness of 0.015” is suggested.



The base heat sink may be of various materials whose shape and size are a function of the individual application and the heat transfer requirements.

**Common Materials**

**Advantages and Disadvantages**

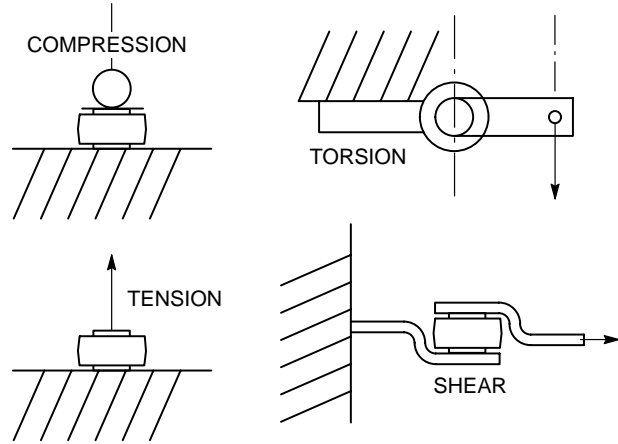
Steel	Low Cost: relatively low heat conductivity
Copper	High Cost: high heat conductivity
Aluminum	Medium Cost: medium heat conductivity. Relatively expensive to plate and not all platers can process aluminum.

Handling of the button during assembly must be relatively gentle to minimize sharp impact shocks and avoid nicking of the plastic. Improperly designed automatic handling equipment is the worst source of unnecessary shocks. Techniques for vacuum handling and spring loading should be investigated.

The mechanical stress limits for the button diode are as follows:

Compression	32 lbs.	142.3 Newton
Tension	32 lbs.	142.3 Newton
Torsion	6-inch lbs.	0.68 Newtons-meters
Shear	55 lbs.	244.7 Newton

**MECHANICAL STRESS**



Exceeding these recommended maximums can result in electrical degradation of the device.

**Soldering**

The button rectifier is basically a semiconductor chip bonded between two nickel-plated copper heat sinks with an encapsulating material of epoxy compound. The exposed metal areas are also tin plated to enhance solderability.

In the soldering process it is important that the temperature not exceed 260°C if device damage is to be avoided. Various solder alloys can be used for this operation but two types are recommended for best results:

1. 95% Sn, 5% Sb; melting point 237°C
2. 96.5% tin, 3.5% silver; melting point 221°C
3. 63% tin, 37% lead; melting point 183°C

Solder is available as preforms or paste. The paste contains both the metal and flux and can be dispensed rapidly. The solder preform requires the application of a flux to assure good wetting of the solder. The type of flux used depends upon the degree of cleaning to be accomplished and is a function of the metal involved. These fluxes range from a mild rosin to a strong acid; e.g., Nickel plating oxides are best removed by an acid base flux while an activated rosin flux may be sufficient for tin plated parts.

Since the button is relatively lightweight, there is a tendency for it to float when the solder becomes liquid. To prevent bad joints and misalignment, it is suggested that a weighting or spring loaded fixture be employed. It is also important that severe thermal shock (either heating or cooling) be avoided as it may lead to damage of the die or encapsulant of the part.

Button holding fixtures for use during soldering may be of various materials. Stainless steel has a longer use life while black anodized aluminum is less expensive and will limit heat reflection and enhance absorption. The assembly volume will influence the choice of materials. Fixture dimension tolerances for locating the button must allow for expansion during soldering as well as allowing for button clearance.

### Heating Techniques

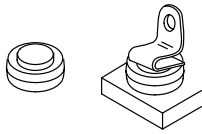
The following four heating methods have their advantages and disadvantages depending on volume of buttons to be soldered.

1. **Belt furnaces** readily handle large or small volumes and are adaptable to establishment of “on-line” assembly since a variable belt speed sets the run rate. Individual furnace zone controls make excellent temperature control possible.
2. **Flame Soldering** involves the directing of natural gas flame jets at the base of a heatsink as the heatsink is indexed to various loading–heating–cooling–unloading positions. This is the most economical labor method of soldering large volumes. Flame soldering offers good temperature

control but requires sophisticated temperature monitoring systems such as infrared.

3. **Ovens** are good for batch soldering and are production limited. There are handling problems because of slow cooling. Response time is load dependent, being a function of the watt rating of the oven and the mass of parts. Large ovens may not give an acceptable temperature gradient. Capital cost is low compared to belt furnaces and flame soldering.
4. **Hot Plates** are good for soldering small quantities of prototype devices. Temperature control is fair with overshoot common because of the exposed heating surface. Solder flow and positioning can be corrected during soldering since the assembly is exposed. Investment cost is very low.

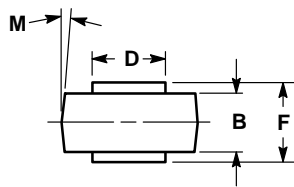
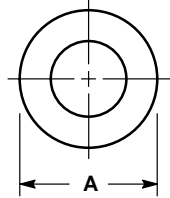
Regardless of the heating method used, a soldering profile giving the time–temperature relationship of the particular method must be determined to assure proper soldering. Profiling must be performed on a scheduled basis to minimize poor soldering. The time–temperature relationship will change depending on the heating method used.



SCALE 1:1

**MICRODE**  
**CASE 193-04**  
**ISSUE L**

DATE 22 SEP 2003



NOTES:

- CASE 193-03 OBSOLETE, NEW STANDARD 193-04.

DIM	MILLIMETERS		INCHES	
	MIN	MAX	MIN	MAX
A	8.43	8.69	0.332	0.342
B	4.19	4.45	0.165	0.175
D	5.54	5.64	0.218	0.222
F	5.94	6.25	0.234	0.246
M	5 °NOM		5 °NOM	

**GENERIC**  
**MARKING DIAGRAM\***



- DEV = Specific Device Code
- A = Assembly Location
- YY = Year
- WW = Work Week

\*This information is generic. Please refer to device data sheet for actual part marking.

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